



STRUCTURAL SYNTHESIS OF ROBOT MANIPULATORS BY USING SCREW WITH VARIABLE PITCH

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Abstract: This paper focuses on the systematic type synthesis of parallel robot manipulators by using new structural formulas based on the screw theory. New structural formulas as a total number of screw in kinematic pairs ($\$$), number of screws with variable pitch ($\tilde{\$}$), total number of screws that represent the contact geometry of lower and higher joint elements (t), mobility equation for robot manipulators (M), dimension of the closed loop (λ), motion of end effector of parallel manipulator (m), number degree of freedom of kinematic pairs (f), refers to find the kinematic structure of robot manipulators realizing a specified motion requirement. Twenty kinematic pairs with structural parameters ($\$, \tilde{\$}, f, t$) are introduced. History of six structural formulas using for structural synthesis of parallel robot manipulators from space and different subspaces are presented as a table with equations, authors, years and some commentaries. The structural synthesis approach is based on the elementary notions of screw theory. Using the proposed of structural formulas approach, families of platform manipulators are constructed from a set of structural units. This paper is appropriate for engineers with interest in robotics, rovers, space docking parallel manipulators and screw theory.

Keywords: *Kinematic pair screws; Motion of end effector; Screws with variable pitch; Dimension of closed loop.*

Introduction. Structural synthesis of robot manipulators is the fundamental concept in robot design. The mobility of robotic mechanical system indicates the number of independent input parameters to solve the configuration of robots. If mobility of the kinematic chain is equal to zero ($M = 0$) and can not be split into several structural groups, we will get a simple structural group. Combining the simple platform (with $n \geq 2$ kinematic pairs) type structural groups with given actuators, we can get parallel platform type robot manipulators needed to define the location (position and orientation) of end effectors. Serial platform manipulators control the motion of the platform, which are connected each others by hinges, branches, legs and other kinematic chains going from the platforms toward the frame. Complex robot manipulators consist of independent branches and legs loops with variable general constraints $\{\lambda_k\}_2^6$. Many platform type robot manipulators use legs with variable general constraints. Therefore structural formulas are used by engineers for design the parallel and serial platform Euclidean robot manipulators with variable general constraints. Structural synthesis of parallel Cartesian platform robot manipulators consists from connecting the simple structural groups constructed in the orthogonal planes to actuators and moving platform.

The history of formulas for structural analysis and synthesis of mechanisms and robotic mechanical systems during the second half of the 19th century, the first and second half of the 20th century and the beginning of 21st century had been

investigated and illustrated in the Table by 38 equations, authors, years and commentaries in the fundamental investigations [1] and in a critical review [2]. Several investigations are described a systematic approach of structural synthesis and analysis of mechanisms by using screw theory. First investigation was given by Mueller [3], where in equations for simple structural group and for kinematic chains were used the number of screw in kinematic pairs. Voinea and Atanasiu [4] and Waldron [5] introduced mobility equation of mechanisms with rank parameter equivalent to screw system of the closed loops. The scientific investigations of structural synthesis and analysis of robot manipulators by using screw theory were more dedicated in the beginning of 21st century. Huang and Li [6] proposed a type synthesis of parallel manipulators with mobility $\{M_i\}_3^5$ by using screw theory. Fang and Tsai [7] developed a problem of structural synthesis and analysis by applying screw theory. They enumerated limb structures for parallel manipulators according to reciprocity of limb twist system and wrench system. Jin et.al. [8] are proposed the structural synthesis and analysis of parallel manipulators by using screw algebra. The design of parallel manipulators based on Plücker coordinates is examined by Gao et.al. [9]. An analytical method of using equivalent screw groups for structural synthesis of over constrained parallel manipulators is described in the study of Zhoo et.al. [10]. Kong and Gosselin [11 – 14] proposed a new way for the type synthesis of parallel manipulators with different type of end effector motions by using screw theory and virtual chain approach.

History of formulas for structural synthesis and analysis of robot manipulators given by author at.al. are presented as 6 several equations (formulas 1-6 in Table 1) with the unique key controlling parameters. In investigation [15] the mobility number, λ , is a characteristic of an independent loop of robot manipulator. In Table 1 (formulas # 1) we have been considered mobility equation which contain mixed independent loops with variable general constraint. The history of new formula [16] about the number of independent loops was done in Table 1(formulas # 2). The number of independent loops in platform manipulators is described by the number of mobile platforms (B), the total number of joints on the mobile platforms (j_b) and the total number of branches between mobile platforms (c_b). In the paper [17] and in the Table 1.1 (formulas # 3) the number of independent loops is described as $L = C - B$, where $C = c_l + c_b$ is sum of legs and branches. A classification of parallel manipulators based on the number of mobile platforms, number of joints on the mobile platforms, number of legs and branches, and types of kinematic pairs are also presented. A new structural formulas for robots (formulas # 4 in the Table 1), working in Cartesian space, having three legs in orthogonal planes, introducing simple structural groups in space $\lambda = 6$ and in subspaces $\{\lambda\}_3^5$, and connected to actuators and to the end effector are introduced. Simple serial platform type structural groups in $\lambda = 3$ and $\lambda = 6$ are presented also in [1]. In the study [18] new structural formulas (formulas # 5 in the Table 1) for parallel and serial platform Euclidean robot manipulators with variable general constraints of branch loops and legs were presented. Selecting the legs of the robot manipulators as moving dyads on Euclidean

planes the direct and inverse task will become easier to solve. The new proposed Euclidean manipulators have several legs, which create Euclidean motions on their own Euclidean planes.

Table 1. Structural formulas for synthesis and analysis of robot manipulators.

№	Equations	Authors	Commentary
1	2	3	4
1.	$1. M = \sum_{i=1}^j f_i - \sum_{k=1}^L \lambda_k$ $2. M = \sum_{i=1}^j f_i - \lambda L$ $3. d = 6 - \lambda$ <p>$\{d\}_0^4$ – general constraint for motion of rigid body in space; L – the number of independent loops; λ – the loop motion parameters; f_i – the DoF of kinematic pairs; j – the number of joints.</p>	<p>F. Freudenstain and R.I. Alizade [15] 1975</p>	<p>1. Mobility equation for mechanisms which contain mixed independent loops with variable general constraint. 2. Mobility equation of mechanisms with the same number of independent, scalar loop closure equations in each independent loop. M is the mobility of mechanisms. λ_k is the dimension of the active motion space.</p>
2.	$1. L = j_b - B - C_B$ $2. M = \sum_{i=1}^j f_i - \lambda(j_B - B - C_B) + q - j_p$ $3. \sum_{i=1}^j f_i = \lambda(j_B - B - C_b)$ <p>B – the number of mobile platforms; j_B – the total number of joints on the mobile platforms; C_b – the total number of branches between mobile platforms.</p>	<p>R.I. Alizade [16] 1988</p>	<p>1. L is the number of independent loops. 2. M is mobility of mechanisms and platform manipulators. 3. Equation for simple structural groups $\{\lambda\}_2^6$, q is excessive over closing constraints, j_p is number of passive DoF in kinematic pairs.</p>
3.	$1. L = C - B$ $2. M = \sum_{i=1}^j f_i - \lambda(C - B)$ $3. \sum_{i=1}^j f_i = \lambda(C - B)$ <p>$C = C_l + C_b$, parameter C is the sum of legs and branches. $C_l = j_B - 2C_b$ C_l – the total number of legs.</p>	<p>R.I. Alizade and C. Bayram [17] 2003</p>	<p>1. New formula for the number of independent loops. 2. Mobility equation of platform robot manipulators. 3. Equation for simple structural groups.</p>
4.	$1. M = (B - C)\lambda + \sum_{i=1}^j f_i + q - j_p$ $2. M = (\lambda + 3) + \sum_{l=1}^{C_l} (d_l - D) + \sum_{l=1}^{C_l} (f_l - \lambda_l) + q - j_p$ <p>$C = C_l + C_b + C_h$</p>	<p>R.I. Alizade, C. Bayram and E. Gezgin [1] 2007</p>	<p>1. Mobility equation for robotic systems. 2. A structural formula of mobility loop–legs equation for parallel Cartesian platform manipulators. d is the constraint parameter of independent loop. D is the number of dimensions of vectors in</p>

	<p>C_h – the number of hinges; $\lambda = 6 - d$; λ – the number of independent location parameters of rigid body in the independent loop; d_l – the number of dimensions of vectors in subspaces of legs. f_l – DoF of the kinetic pairs on the leg.</p>		<p>Cartesian space.</p>
<p>5.</p>	<p>1. $M = \lambda + j_h + \sum_{L=1}^n (f_L - \lambda_L)$ $+ \sum_{l=1}^{c_l} (f_l - \lambda_l) + q - j_p$ 2. $m = \lambda + c_l + j_h + \sum_{l=1}^{c_l} (d_l - D) + \sum_{L=1}^n (f_L - \lambda_L)$ j_h – the number of hinges between platforms; f_L – DoF of kinematic pair on the branch-loop. λ_L – the motion of rigid body in branch-loop.</p>	<p>Rasim Alizade, Fatih Cemal Can, Erkin Gezgin [18] 2008</p>	<p>1. The general structural formula of serial-parallel Euclidean robot manipulators with variable general constraints. 2. The general formula for motion of platforms. D – dimensions of vectors ($D = 3$ for space R^3, $d = 2$ for plane R^2)</p>
<p>6.</p>	<p>1. $\\$ = f - \tilde{\\$} + t$ 2. $M = \sum_{f=1}^{\lambda-1} fP_f - \sum_{k=1}^L \lambda_k + q$ 3. $M = \sum_{f=1}^{\lambda-1} fP_f - \lambda(C - B) + q$ 4. $M = \lambda + \sum_{l=1}^{c_l} \left(\sum_{f=1}^{\lambda-1} fP_f - \lambda_l \right)$ $+ \sum_{b=1}^{L_b} \left(\sum_{f=1}^{\lambda-1} fP_f - \lambda_b \right) + j_h$ 5. $m = \lambda + c_l + j_h + \sum_{l=1}^{c_l} (d_l - D)$ $+ \sum_{b=1}^{L_b} \left(\sum_{f=1}^{\lambda-1} fP_f - \lambda_b \right)$ 6. $M = \lambda + \left(\sum_{f=1}^{\lambda-1} fP_f - \lambda_l \right) c_l + \sum_{f=1}^{\lambda-1} (fP_f - \lambda_b) L_b$ $+ j_h$ 7. $m = \lambda + c_l + j_h + (d_l - D)c_l$ $+ \left(\sum_{f=1}^{\lambda-1} fP_f - \lambda_b \right) L_b$ t – represents the number of screws that describe the contact geometry of joint elements. $t = 2$ – contact elements on surface; $t = 3$ – contact elements on line; $t = 4$ – contact elements on points;</p>	<p>Rasim Alizade 2017</p>	<p>1. Total screws in kinematic pair. 2. Mobility equation for robot manipulators with variable loop motion parameters. 3. Mobility equation with the same dimension in each independent loop. 4. Structural formula for Euclidean platform type robot manipulators with variable general constraints. 5. Structural formula that describe the motions of end effector on the parallel robot manipulators. 6. Mobility equation for Euclidean manipulators with constant general constraint. 7. Motion of end effector of Euclidean manipulator with constant general constraint.</p>

The motion of the platform is defined by three independent curves of three

platform points moving on three Euclidean reference planes. The general formula for motion of platforms is given also. To create new robot manipulators, simple platform structural groups with variable general constraints were considered.

This study enunciates screw system with variable pitch for the prismatic and cylindrical joints. Applying concepts the number of independent screw, number of screw with variable pitch, number of screws and motions for lower and higher kinematic pairs (Table 1.6.1) become possible to provide the structural characteristics of 20 kinematic pairs (Table 2). Two new general mobility equations for robot manipulator with mixed and the same dimension of closed loop are presented in the work (Table 1.6.2 and 1.6.3).

Applying above mobility equations for structural synthesis problem the new wheeled robot that are called as “Rover” had been designed. This rover consists from moving platform and two suspensions with six wheels connected to the platform. Each suspension consist from paired two Chebyshev lambda mechanisms called bogie and one dyad called rocker. Two parallel suspensions are connected by a differential gear mechanism (Fig.2).

The problem of structural synthesis of parallel wheeled rover was solved by using structural formulas 3 and 5 from Table 1.6. In current study, new structural formulas are introduced for parallel Euclidean platform robot manipulators (Table 1.6) with variable and fixed general constraints. Structural synthesis task of four new design Euclidean docking parallel manipulators with three, four, five and six legs were solved for spacecraft (Table 3). Furthermore, new 6DoF Euclidean docking manipulators of Spacecraft and their structural classification with the same general constraints of each legs are presented. Also, in the Table 3 were depicted the structural parameters, kinematic structures, motion of platform, number of legs and 3D drawing of new docking parallel manipulator of Spacecraft. It is clear that the 6DoF Euclidean parallel manipulator with different number of legs will better generate the given position and orientation of moving platform.

Introduction to screw with variable pitch. The structural and kinematic analysis and synthesis problem have been studying with the goal of identified new methods for composing robot manipulators capable of performing various prescribed positions and orientations of the end effectors. Screw with variable pitch can represent the prismatic joint, P , with the variable pitch parameter $\mu_P = \infty$, and also the cylindrical joint $C(RP)$ with variable pitch $\mu_C = (\infty; 0)$ that describe a rotation motion ($\mu_R = 0$) and translation motion $\mu_P = \infty$.

As shown in Fig. 1, the location of a rigid body (RB) of the cylindrical joint can be described by the three parameters for position (x, y, z) and three independent parameters (d, α, θ) for orientation. Let coordinate system A and was then translated parallel to the point B_1 (Fig. 1a). The position of point B_1 is described by vector $\vec{r}(x, y, z)$. Next, the system B_2 that is initially aligned with system B_1 is rotated by the twist angle α about the x_{B_1} axis. Following this the coordinate system B_2 of rigid body is translated along the z_{B_2} axis by a distance d . Lastly the coordinate system B

that was firstly aligned with the system B_2 is rotated by the angle θ around z_B , so we will get orientation of the coordinate system $Bx_By_Bz_B$.

Transformation of one coordinate system B to a reference coordinate system A correspond to the transformation of screw $\$,$ when the relative position and orientation of the pair of screws are known (Fig. 1a). By using homogeneous coordinates the transformation of the system will be represented by 4×4 matrix as:

$${}^A T_B = \begin{bmatrix} 1 & 0 & 0 & x \\ 0 & 1 & 0 & y \\ 0 & 0 & 1 & z \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & c\alpha & -s\alpha & 0 \\ 0 & s\alpha & c\alpha & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & \tilde{d} \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} c\tilde{\theta} & -s\tilde{\theta} & 0 & 0 \\ s\tilde{\theta} & c\tilde{\theta} & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \\ = \begin{bmatrix} c\tilde{\theta} & -s\tilde{\theta} & 0 & x \\ s\tilde{\theta}c\alpha & c\tilde{\theta}c\alpha & -s\alpha & y - \tilde{d}s\alpha \\ s\tilde{\theta}s\alpha & 0 & c\alpha & z + \tilde{d}c\alpha \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (1)$$

where: $S\theta$ and $C\theta$ represent the sine and cosine of θ , and $S\alpha$ and $C\alpha$ represent the sine and cosine of α .

Knowledge of these six parameters $(x, y, z, \alpha, d, \theta)$ completely defines the position and orientation of the B coordinate system attached to the rigid body of the cylindrical joint and measured with respect to the A coordinate system as shown in Eq.(1). The location of rigid body reduce a single vector $\bar{S} // \bar{Z}_B$ and a couple moment $\bar{U} // \bar{Z}_{B_1}$ at point B_1 with a twist angle α (Fig. 1b). The couple moment $\bar{U} = \bar{r} \times \bar{S}$ may be resolved into two components: one $\bar{U}_{//}$ collinear with joint vector \bar{S} in the direction by twist angle α . The perpendicular component \bar{U}_{\perp} will rotate rigid body around cylindrical joint vector \bar{S} by rotation angle θ , so $\tilde{\theta} = \theta \bar{S}$.

The twist angle α was defined between vectors \bar{S} and \bar{U} (Fig. 1b) measured in a right-hand sense about \bar{x}_{B_1} . The rotation angle θ was defined between \bar{x}_{B_2} and \bar{x}_B measured in a right hand sense about \bar{S} (Fig. 1a). It is known that, there are two distinct angles between 0 and 2π that will have the same cosine value. So, the expressed for the cosine and sine of α and θ can be expressed by Eqs. (2):

$$\begin{cases} \cos \alpha = \bar{U} \cdot \bar{S} \\ \sin \alpha = (\bar{U} \times \bar{S}) \cdot \bar{x}_{B_1} \end{cases} \begin{cases} \cos \theta = \bar{x}_B \cdot \bar{x}_{B_2} \\ \sin \theta = (\bar{x}_B \times \bar{x}_{B_2}) \cdot \bar{Z}_B \end{cases} \quad (2)$$

As shown in Fig. 1, the axes of the cylindrical joint \bar{S} and a couple moment $\bar{U}_{//}$ has the same line. Thus the combination of a collinear vector \bar{S} and a couple moment $\bar{U}_{//}$ is called a screw or wrench.

So, the screw with variable pitch has both a translation d and rotation θ about the axis \bar{S} described by twist angle α . Parameters d , θ and α are independent parameters of rigid body motion respect to screw $\tilde{\$}$ with variable pitch.

Two collinear vectors \bar{S} and $\bar{U}_{//}$ uniquely determine the position and orientation of the screw with variable pitch.

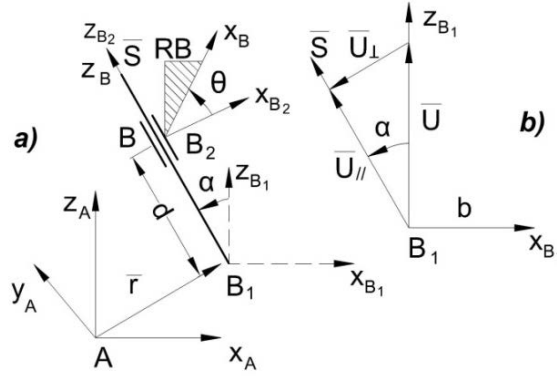


Fig. 1. Kinematic model of cylindrical joint

\bar{S} is an axis vector and $\bar{U}_{//}$ is moment of screw \tilde{S} , where \bar{S} defines the direction of motion of screw \tilde{S} and moment $\bar{U}_{//}$ determines the rotation around the axis. Unit vector \bar{S} and moment $\bar{U}_{//}$ can be introduced as dual vector that is called a screw with variable pitch:

$$\tilde{\$} = \bar{S} + \varepsilon(\bar{U}_{//} + \tilde{\mu}\bar{S}) \quad (3)$$

where $\varepsilon^2 = 0$ is operator of Clifford.

The ratio of joint position d and joint rotation θ in cylindrical joint reduce to the following variable pitch:

$$\tilde{\mu} = \frac{d}{\theta} \quad (4)$$

As shown in Fig. 1b the rotation moment in cylindrical joint reduce to expression as follow:

$$\bar{U}_{//} = \bar{U} \cdot \cos \alpha = (\bar{r} \times \bar{S}) \cos \alpha \quad (5)$$

Hence, using Eqs. (3 ÷ 5) the vectors \bar{S} and resultant couple moment \bar{U} describing location of a rigid body with cylindrical joint can be described as a screw with variable pitch:

$$\tilde{\$} = \left[\begin{array}{l} \bar{S} \\ (\bar{r} \times \bar{S}) \cos \alpha + \tilde{\mu}\bar{S} \end{array} \right] \quad (6)$$

So, as shown in Eq. (6), six independent components $(x, y, z, \alpha, d, \theta)$ describe the location of screw with variable pitch. As shown in Eq. (7) the couple moment \bar{U} of the screw with variable pitch is:

$$\bar{U} = (\bar{r} \times \bar{S}) \cos \alpha + \tilde{\mu}\bar{S} \quad (7)$$

Since the screw axis and its moment are in orthogonal planes and unit of screw with variable pitch $|\tilde{\$}| = 1$, so

$$\bar{S} \cdot (\bar{r} \times \bar{S}) = 0 \quad \text{and} \quad \bar{S} \cdot \bar{S} = 1 \quad (8)$$

Multiplying both side of Eq.(7) to the vector \bar{S} we get the following equation:

$$\bar{S} \cdot \bar{U} = (\bar{r} \times \bar{S}) \cdot \bar{S} \cos \alpha + \tilde{\mu}\bar{S} \cdot \bar{S} \quad \text{or} \quad \tilde{\mu} = \frac{\bar{S} \cdot \bar{U}}{\bar{S} \cdot \bar{S}} \quad (9)$$

For revolute, prismatic, screw and cylindrical joints the parameters of pitch to Eq.(8) can be described as follows:

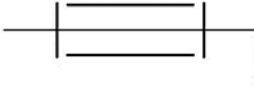
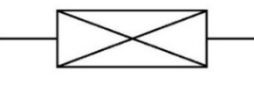
$$\mu_R = 0, \quad \mu_{\$} = \frac{d}{\theta}, \quad \tilde{\mu}_p = \infty, \quad \tilde{\mu}_C = \{0, \infty\}.$$

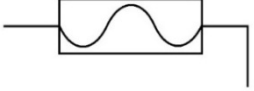

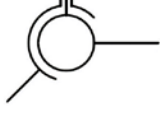
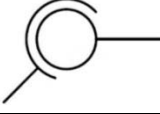
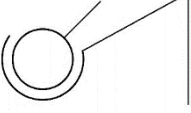
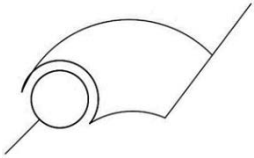
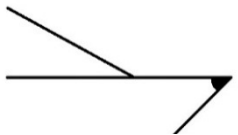
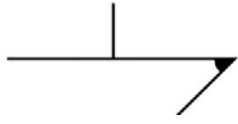
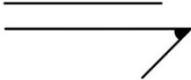
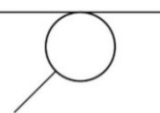
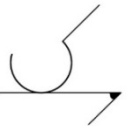
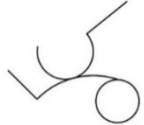
Structural formulas for robot manipulators by using screw theory. The design problem of robot manipulators are a valuable task for structural synthesis. It is known that over constraint robot manipulator must satisfy the geometry of angular and linear constraints that correspond to the geometry of kinematic pairs moving in subspaces. The goal of structural synthesis by using screw theory are identified new methods for composing robot manipulators capable of performing various prescribed functions, position and orientations of end effectors. It is required to form a new structural formula for robot manipulators by using screw theory allows to solve the structural synthesis with variable general constraints including platforms, hinges, legs and branch loops with different ranks, that is introduced from different subspaces and spaces.

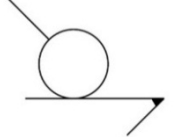
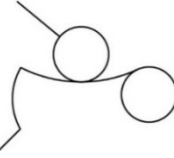
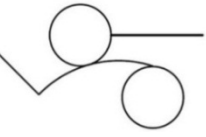
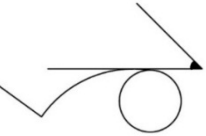
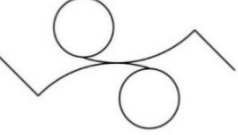
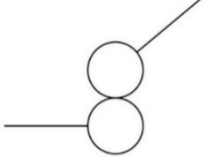
It is known that two rigid bodies attached to each other by surfaces are formed lower kinematic pairs, otherwise if contact geometry of two rigid bodies is line or a point are formed higher kinematic pairs. Due to the fact that the unconstrained space has dimension $\lambda = 6$ with independent motions 3R3P, but dimension of over constraint subspaces is $\lambda = 2 \div 5$ with different angular and linear or just angular conditions in the loops of robot manipulators. Usually kinematic pairs need constraints $c = 1 \div 5$ in order to be defined properly degree of freedom $f = \lambda - c$. Each kinematic pair has input and output link screws and joint independent screws $\$$ with constant pitch μ , however some joints with translation motions has additional variable screws $\tilde{\$}$ with variable pitch $\tilde{\mu}$.

The simple planar surface can be represented by two parallel screws $\underline{\$}_1 \underline{\$}_2$ or two orthogonal screws $\underline{\$}_1^\perp \underline{\$}_2$, so for lower kinematic pairs number of screws $t = 2$. The intersection of two planar surfaces $\underline{\$}_1 \underline{\$}_2$ and $\underline{\$}_2 \underline{\$}_3$ will be result in a line represented by $\underline{\$}_1 \underline{\$}_2 \underline{\$}_3$ or as $\underline{\$}_1^\perp \underline{\$}_2^\perp \underline{\$}_3$ so for higher kinematic pair with line contact of elements the number of screws $t = 3$. The intersection of three planar surfaces that will be result in a point can be represented by four screws $\underline{\$}_1 \underline{\$}_2 \underline{\$}_3 \rightarrow \underline{\$}_2^\perp \underline{\$}_4$ or as $\underline{\$}_1^\perp \underline{\$}_2^\perp \underline{\$}_3^\perp \underline{\$}_4$, so for higher kinematic pair with point contact of elements the number of screws $t = 4$. Elements of the structural bonds can be illustrated as " $\underline{\quad}$ " describe the parallel of screws and " \perp " describe the perpendicular of screws.

Table 2 Joints kinematic parameters.

№	Name	Symbol	Kinematic parameters				Diagram
			t	f	$\tilde{\$}$	$\$$	
1	2	3	4	5	6	7	8
1	Revolute	R	2	1	0	3	
2	Prismatic	P	3	1	1	3	

3	Screw	H	2	1	0	3	
4	Cylindrical	C	2	2	1	3	
5	Sphere with finger	S_f	2	2	0	4	
6	Spherical	S	2	3	0	5	
7	Sphere in cylinder slot	S_{cs}	3	4	1	6	
8	Sphere in torus slot	S_{ts}	3	4	0	7	
9	Plane to slope line	$F_{/L}$	4	4	1	7	
10	Plane to perpendicular line	$F_{\perp L}$	4	3	1	6	
11	Plane to parallel lines	$F_{//L}$	3	4	2	5	
12	Line to Sphere	L_S	4	4	1	7	
13	Cylinder to plane	C_F	3	4	2	5	
14	Cylinder to torus	C_t	4	4	1	7	

15	Sphere to plane	S_F	4	5	2	7	
16	Hyperboloid to Sphere	H_S	4	5	2	7	
17	Sphere to Torus	S_t	4	5	2	7	
18	Torus to plane	T_F	4	5	2	7	
19	Torus to torus	T_t	4	5	2	7	
20	Sphere to sphere	S_S	4	5	2	7	

The usage of recurrent screws in the study of kinematic pairs can clarify the motion concept easily. From this point of view the number of independent screws in kinematic pairs can be introduced as follow:

$$\$ = f - \tilde{\$} + t \quad (9)$$

where:

$\tilde{\$}$ = number of screws with variable pitch;

t = number of screws of lower ($t = 2$) or higher kinematic pairs ($t = 3$ for line and $t = 4$ for point contact of elements);

f = degrees of freedom of relative motion permitted at joint.

The twenty kinematic pairs of robot manipulators in all types, symbols, kinematic parameters and their diagrams are shown in Table 2. Using Eq.(9) and (1.1) from Table 1 we can introduce a new general mobility equation for mechanisms with mixed dimensions of closed loops as:

$$M = \sum_{f=1}^{\lambda-1} f P_f - \sum_{k=1}^L \lambda_k + q \quad (10)$$

where: λ_k = number of independent, scalar, loop closure equations associated with k-th independent loop;

P_f is the number of f mobility joints. $f = \$ + \tilde{\$} - t$ is DoF at joint;

q = number of depended constraint equations.

As show in Table 1, the number of independent loops $L = c - B$, so mobility Eq. (10) can be introduced as mobility equation for robot manipulators with the same number of independent, scalar loop closure equation in each independent loop:

$$M = \sum_{f=1}^{\lambda-1} fP_f - \lambda(C - B) + q \quad (11)$$

where: $C = c_l + c_b$ is the sum of legs and branches;

B = number of mobile platforms.

The overall performance of robots and rovers are usually constructed from the multiple platforms, hinges leg and branch loops with variable general constraint parameters, describing the location of rigid body. These robots and rovers can be affected by the topology of their possible mechanical structures. The motions (rotation and translation) of rigid links and platforms of the manipulators could be described in space R^3 and in plane R^2 with dimensions of vectors $D = 3$ and $D = 2$ in reference frame respectively. The location of rigid body in the three dimensional space R^3 can be obtain by Euclidean motions of the two dimensional subspaces R^2 . It is known that the location of rigid body in space R^3 can be determined minimum by three independent curves of the three points of moving rigid body. Let there are dyads kinematic chains on each Euclidean “ $3 \leq \text{planes} \leq 6$ ”. If these kinematic chains of Euclidean planes are joined to the moving rigid body by spherical or spherical-torus kinematic pairs, so we will attain location of the rigid body in the three dimensional space R^3 .

The general structural formula for parallel-serial Euclidean platform type manipulators with variable general constraints [18] including hinges (j_h), leg (l) and branch (L_b) loops can be also formulated in the form as (Table 1):

$$M = \lambda + \sum_{l=1}^{c_l} \left(\sum_{f=1}^{\lambda-1} fP_f - \lambda_l \right) + \sum_{b=1}^{L_b} \left(\sum_{f=1}^{\lambda-1} fP_f - \lambda_b \right) + j_h \quad (12)$$

where: λ is the dimension parameter of moving platform; λ_l and λ_b are dimension parameters of leg and branch loops; j_h is the number of hinges between platforms.

The structural formula for motion [18] of platforms that are created by mechanical system from different Euclidean planes can be introduced in the following form (table 1):

$$m = \lambda + c_l + j_h + \sum_{l=1}^{c_l} (d_l - D) + \sum_{b=1}^{L_b} \left(\sum_{f=1}^{\lambda-1} fP_f - \lambda_b \right) \quad (13)$$

where d_l is the number of dimensions of vectors of the legs in Euclidean planes;

D is the number of dimensions of vectors in the reference frame.

If the number of independent scalar leg-closure equations identical in each Euclidean planes and identical in each branch loops, the general structural formula (12) for Euclidian manipulators can be defined as

$$M = \lambda + \left(\sum_{f=1}^{\lambda-1} fP_f - \lambda_l \right) c_l + \sum_{f=1}^{\lambda-1} (fP_f - \lambda_b) L_b + j_h \quad (14)$$

The general formula for motion of end effector of manipulator (13) with the same dimensions of Euclidean manipulator legs and branch-loops can be given in the following from:

$$m = \lambda + c_l + j_h + (d_l - D)c_l + \left(\sum_{f=1}^{\lambda-1} fP_f - \lambda_b \right) L_b \quad (15).$$

Structural Synthesis of 6DoF Parallel Docking Manipulator of Spacecraft.

In space flights the orbital docking system is used. The use of an orbital station with two docking units ensures a rigid connection with the formation of a hermetically sealed tunnel. A large number of interacting mechanisms are concentrated in the docking aggregates. The multi-functionality of the working bodies requires the solution of the problem of the structural synthesis of spatial manipulators of coupling aggregates. Since the mechanisms operate in open space, it is therefore necessary to develop new manipulators, nodes and elements of kinematic pairs. Structural parameters, kinematic structure, motion of platform and 3D drawing of the spaces docking manipulators $6RRS_t$ is depicted in Table 3. Controllable space vehicles are brought to a touch with a certain speed and position, after which the process of docking with a spatial manipulator of a parallel structure begins, which ends with a rigid connection of two docking units. After the end of the flight, an undocking takes place by releasing the mechanical connections of the docking device of the platform manipulator from the orbital station (Table 3.1).

When docking it is required that the coaxial position of the docking assemblies and the zero linear and angular velocities be maintained. The possible values of the relative coordinates and their first derivatives in the case of mechanical contact are called the initial conditions of the docking. Deviations from the co-axial position (Table 3.2) are determined by the linear coordinates δ_y , δ_z and planar angles δ_ψ , δ_φ , δ_θ . The total deviations of the docking units from the co-axial position are added from the errors: unit settings, measurements and control dynamics. Electromechanical docking devices have been created to reduce errors based on electromechanical dampers. With the damping, the brake robot can accelerate in a unit of millisecond to a speed of several thousand revolutions per minute.

The new four proposed Euclidean docking manipulators have identical legs as plane dyads RR as shown in Table 3.3a. Each end of dyads connect to the moving platform by spherical-tours pairs. Kinematic pair with 4DoF is introduced as sphere in torus slot pair S_{ts} that perform three rotations and one circular translation (Table 3.3 b). Note that, end points of each dyads respect to the fixed reference frame (Table 3.3 c) define the curve of one point of the platform in the reference Euclidean plane. Three legs RRS_{ts} of the moving platform defines the three reference Euclidean planes (Table 3.3 c) that are located under an angle of 120° . It is known that the location of

the moving rigid body in space can be defined by minimum three independent curves of three rigid body points moving on three Euclidean reference planes.

Since the Euclidean parallel docking manipulator consist of a movable platform and legs, then the number of branch-loops $L_b = 0$, hinges $j_h = 0$ and $\lambda_l = const$, so Eq. (14) takes the form:

$$M = \lambda + \left(\sum_{f=1}^{\lambda-1} f P_f - \lambda_l \right) c_l \quad (16)$$

In the same way when $L_b = 0$, $j_h = 0$ and $d_l = const$, then the formula (15) for motion of platform of Euclidean docking manipulator can be written in the form

$$m = \lambda + (1 + d_l - D) c_l \quad (17)$$

Example 1. Design a parallel Euclidean docking robot manipulator with $\lambda = 6$, $\lambda_l = 6$, $c_l = 6$, $M = 6$. Find both the number and kind of kinematic pairs on each leg. Also, find the motion of docking platform.

By using Eq.(16) total DoF and kind of kinematic pairs of the legs can be calculated as

$$(M - \lambda) c_l^{-1} + \lambda_l = \sum_{f=1}^5 f P_f \quad or$$

$$6 = P_1 + 4P_4, \quad or \quad P_1 = 2 \quad and \quad P_4 = 1$$

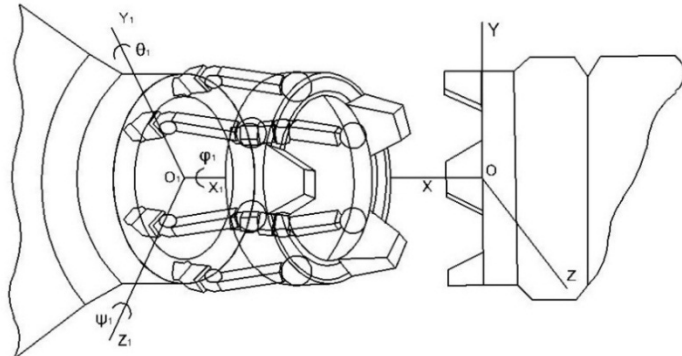
so that, in the designed docking manipulator, each leg will consist of two kinematic pairs with one degrees of freedom (revolute pairs RR) and one kinematic pair with four degrees of freedom (sphere in torus slot pair S_{ts}). By using Eq.(17), the motion of the docking platform will be $m = 6$, it means motion of platform will $R_x, R_y, R_z, P_x, P_y, P_z$.

Kinematic structure with different structural parameters of Euclidean docking robot manipulator with six legs is shown in Table 3.1.

The above procedure can be used for Euclidean docking robot manipulators with three, four and five legs.

The result of the new Euclidean docking robot manipulators are shown in Table 4. Elements of the structural bonds can be illustrated as: Restangle (\square):

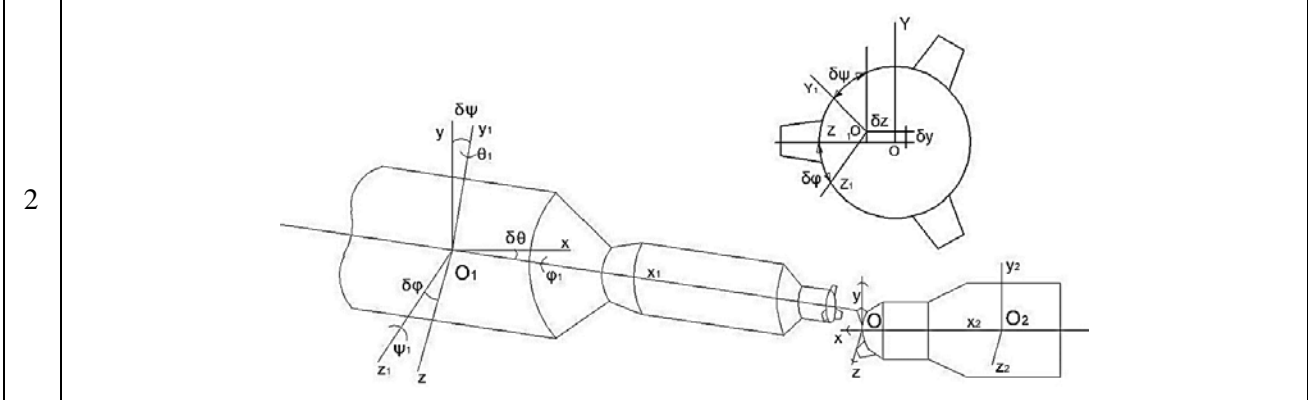
Table 3. Parallel Euclidean Platform Spacecraft Docking Manipulator.

№	The new Spatial Docking Manipulator of Spacecraft.
1	

Structural synthesis of robot manipulators by using screw with variable pitch

$\overline{RR} - \overline{S_t S_t S_t S_t S_t} - \overline{RR}$	$R_x, R_y, R_z, P_x, P_y, P_z$	α	λ_l	c_l	leg. $P_1 = 2$ $P_4 = 1$	d_l 2,2,2 2,2,2	m_p 6	M 6
1	2	3	4	5	6	7	8	9

The Deviations of the Docking Units.



a	Dyad in reference Euclidean plane.	b	Sphere in torus slot pair	c	The three platform points on three Euclidean planes.
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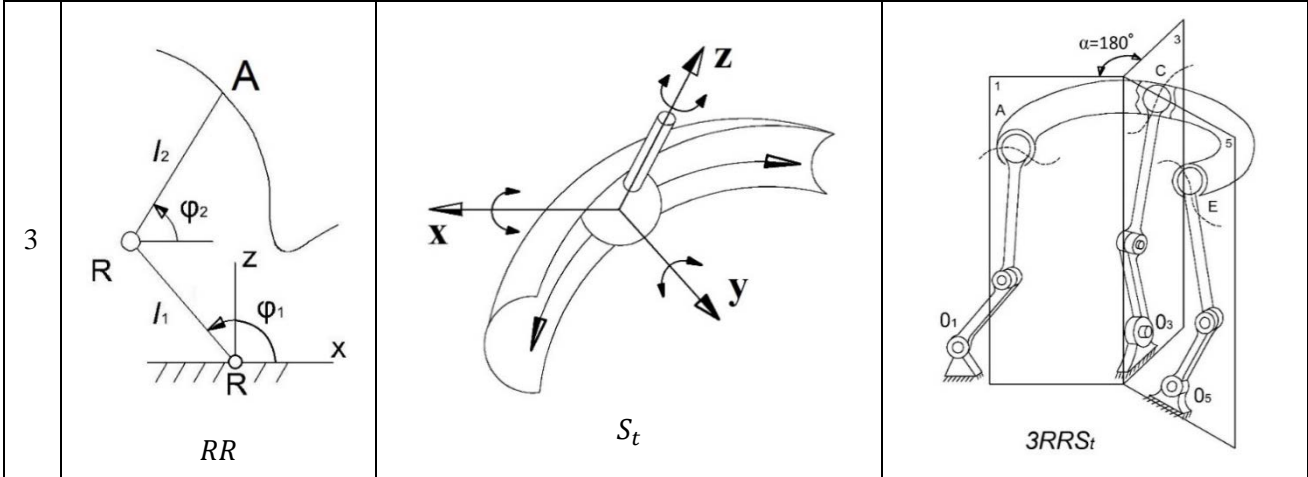
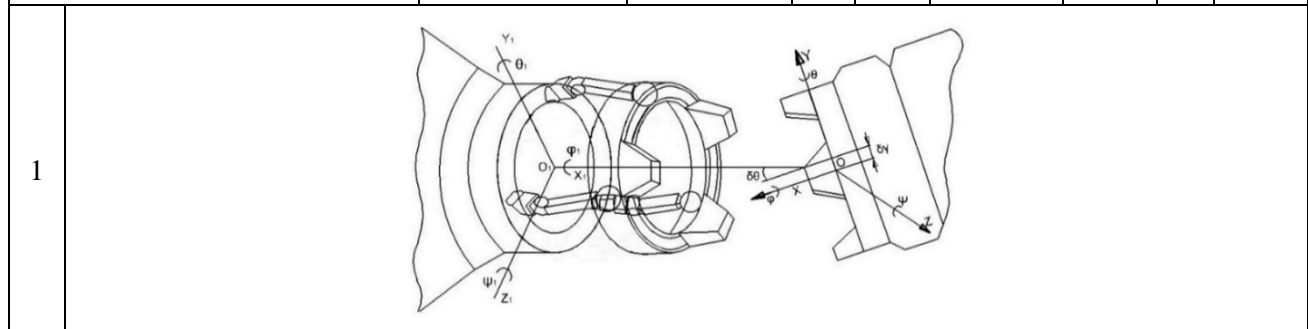
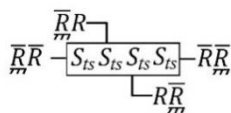
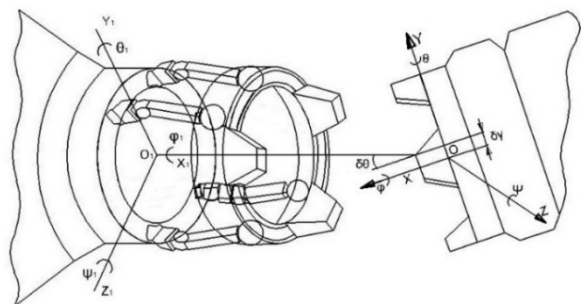
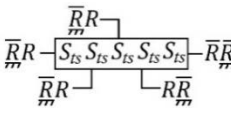
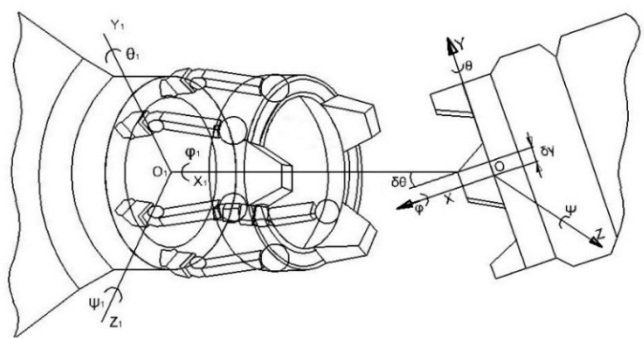


Table 4. New 6DoF Parallel Docking Manipulators of Spacecraft.

Structural bonding	Illustration							
	Motion of platform	Angle between Euclidean planes	λ_l	c_l	leg. $\sum f P_f$	d_l	m_p	M
1	2	3	4	5	6	7	8	9
$\overline{RR} - \overline{S_{ts} S_{ts} S_{ts}} - \overline{RR}$ $\overline{R R}$	$R_x, R_y, R_z, P_x, P_y, P_z$	120°	6	3	$P_1 = 2$ $P_4 = 1$	2,2,2	6	6
1	2	3	4	5	6	7	8	9



1	2	3	4	5	6	7	8	9
	$R_x, R_y, R_z, P_x,$ P_y, P_z	90°	6	4	$P_1 = 2$ $P_4 = 1$	$2, 2, 2,$ 2	6	6
2								
1	2	3	4	5	6	7	8	9
	$R_x, R_y, R_z, P_x,$ P_y, P_z	72°	6	5	$P_1 = 2$ $P_4 = 1$	$2, 2, 2,$ $2, 2$	6	6
3								

describes moving platform with spherical-torus pairs S_t .

Platform leg $(-, L)$: connection of the spherical-torus pairs on the moving platform with pairs of the legs.

\overline{RR} : input joint on fixed frame.

\overline{R} : input joint on moving frame.

Structural Synthesis of Wheeled Robots. It is obvious that wheeled robot have been developed for Mars and Moon surface. First we consider the definition of wheeled robot: “A wheeled robot is an autonomous system capable of traveling a terrain with natural or artificial obstacles”. As shown in Fig. 2.1 kinematic structure of wheeled robot has six wheels with symmetric structure for both sides. Each side has three wheels which are connected to each other by the main linkage and two loops kinematic chain. Main linkage called rocker that has two joints, where first joint connected to back wheel and second joint assembled to platform. The rocker is kinematic chain where the second path of link connected rigidly to another linkage system with two wheels. The second linkage system is called bogie (Fig. 2.2). So, rocker-bogie kinematic chain is called suspension system. Wheeled rough terrain mobile robots are called as “Rover”. Rovers can carry more weight with high-speed, easy navigation and more precisely can be calculated position and orientation. First rover was “Lunakhod” and second rover was six wheeled suspension system, which

connects the wheels to the platform. This connection are linkage mechanisms, damping and complex spring.

The new bogie mechanism consists of two Chebyshev lambda mechanisms which are connected symmetrically. Paired two lambda mechanisms are used as motion generation mechanisms, where couplers are input links. To move the coupler points M_1 and M_2 along a line sufficiently and necessary to fulfil the design relation: $3d - a = 2b$. The length of parametre d can be changed according to relation $1,55a \leq d \leq 3a$ (Fig. 2.1). The same second suspension kinematic chains are assembled in opposite side of moving platform. Right and left suspensions are connected to each other by a differential gear mechanism (Fig. 2). When one side climbing over obstacle, this mechanism rotates the platform around the rocker joints by average angle of two sides (Fig. 2.1). So, the wheeled robot is equipped with six wheels and possibly a manipulator setup mounted on the platform for handling of work pieces, tools or special devices. On inclined surface the moving rover can hold the main platform horizontal. Navigation gets easier by this feature of rover. Rovers are driven by commands which are sent from ground operators after tested in 3D computer simulation. Some of the critical motions such as climbing high slope, new rover designs are needed to more flexible duaring field operation.

Example 2. Design a parallel wheeld rover with six legs $c_l = 6$, three branch $c_b = 3$ and one moving platform $B = 1$ (Fig. 2.1). The dimension parameter of each independent loops on the left and right suspensions $\{\lambda_k\}_1^8 = 3$ (Fig. 2.2). The number of kinematic pairs with one DoF in the left and right suspensions $P_1 = 30$. Two suspensions kinematic chains are connected by differential gear mechanism. Find the number of motors for parallel whelled rover. Also, find the motion of the rover's platform.

First, we define the number of independent loops (Table 1.3):

$$L = C - B = c_l + c_b - B = 6 + 3 - 1 = 8.$$

Using Eq. (11) total DoF of parallel wheeled rover can be calculated as

$$\begin{aligned} M &= \sum_{f=1}^5 f P_f - \lambda(C - B) = P_1 - \lambda(c_l + c_b - B) = \\ &= 30 - 3(6 + 3 - 1) = 6. \end{aligned}$$

By using Eq.(17), the motion of the moving rover's platform can be defined as

$$m = \lambda + (1 + d_l - D)c_l = 6 + (1 + 2 - 3) = 6.$$

Thus, the problem of the structural synthesis of the wheeled rocker-bogie mechanism is solved and it is introduced in Fig.2. Spring and damper application to double lambda bogie good solution for high-speed off-road vehicles.

Rocker-Bogie suspensions can be used also for vehicles with a larger number of wheels. An example of a layout for an 8-wheeler each suspension will consist from four motion generation Chebyshev lamda mechanisms with the four given wheels. In this case the vehicle may be summetrical and it can run in both direction without any difference.

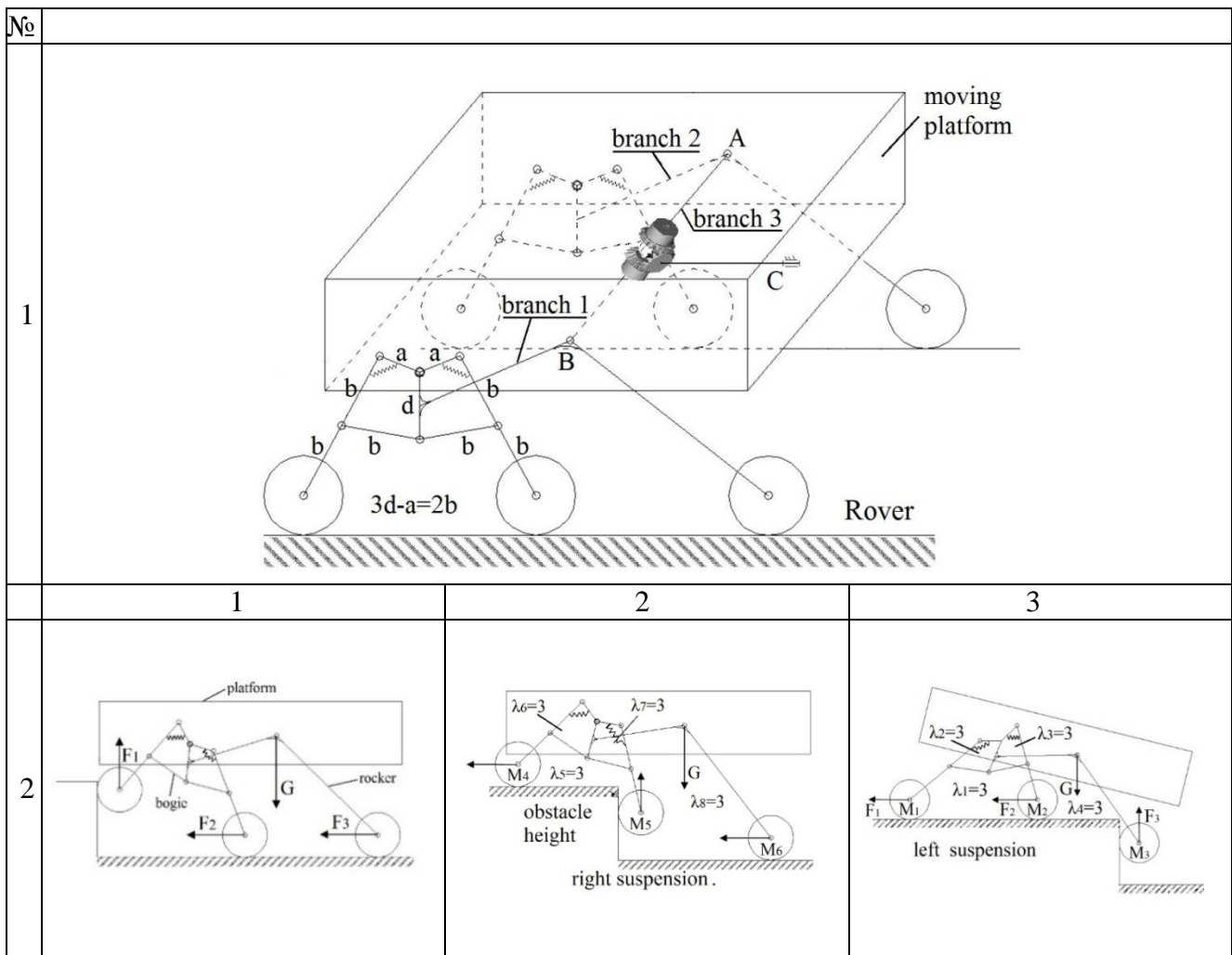


Fig. 2. Kinematic model of rocker-bogey mechanism.

Conclusion. The problem of structural synthesis of the robot manipulators with variable general constraint of the legs and closed loops can be difficult and complex task depends on the DoF and motion of an end-effector concept. It is described a new structural formula of kinematic pairs for robot manipulators by using screw with variable pitch. From this point the twenty kinematic pairs are shown with types, symbols, kinematic screw parameters and their diagrams. It were introduced two new general mobility equations for mechanisms with mixed or fixed dimensions of close loops. The general structural formula for Euclidean manipulators with variable or identical general constraints are introduced. The new structural formula for motion of end effector of robot with legs from different Euclidean planes were considered. Four new Euclidean 6DoF parallel docking manipulators of Spacecraft were reviewed and synthesized. Finally, by using sistematic process of structural synthesis by using for mobility of robot and motion of moving platform were developed to create new structure of wheeled robot-rover for Mars and Moon surface.

REFERENCES:

- [1]. Alizade R.I., Bayram C., Gezgin E., *Structural Synthesis of serial platform manipulators*, IFToMM J., Mechanism and Machine Theory 42, 580-599, (2007).
- [2]. Gogu G., *Mobility of mechanisms: a critical review*, IFToMM J. Mech. Mach. Theory 40, 1068-1097, (2005).
- [3]. Muller R., *Die zwanglanfigkeit kinematische ketten*, Unpublished dissertation (1920), as quoted in K. Federhofer: *Graphische Kinematic and Kinetostatic*, Springer, Berlin, (1932).
- [4]. Voinea R., Atanasiu M., *Contributions a la theorie geometrique des vis*, Bull. Inst. Politech. Bucuresti XXI (3) (1959).
- [5]. Waldron K.J., *The constraint analysis of mechanisms*, J. Mech. 1, pp. 101-114, (1966).
- [6]. Huang Z., Li Q.C., *General methodology for type synthesis of symmetrical lower-mobility parallel manipulators and several novel manipulators*, Int. J. Robot. Res. 21, pp. 131-145, (2002).
- [7]. Fang Y., Tsai L.W., *Structure synthesis of a class of 4-DoF and 5-DoF parallel manipulators with identical limb structures*, Int. J. Robot. Res. 21, pp. 799-810, (2002).
- [8]. Jin Y., Chen I.M., Yang G., *Structure synthesis and singularity analysis of a parallel manipulator based on selective actuation*. Proceeding of the International Conference on Robotics and automation (2004) 4533-4538.
- [9]. Gao F., Li W., Zhao X., Jin Z., Zhao H., *New Kinematic structures for 2-5 DoF parallel manipulator designs*, IFToMM J, Mechanism and Machine Theory 37, pp. 1395-1411, (2002).
- [10]. Zhao T. S., Dai J. S., Huang Z., *Geometric analysis of over constrained parallel manipulators with 3-4 DoF*, ASME Journal Series C, Vol. 45, No. 3, pp. 730-740, (2002).
- [11]. Kong X., Gosselin C. M., *Type Synthesis of 3T1R 4-DoF parallel manipulators based on screw theory*, IEEE Transactions on Robotics and Automation, Vol. 20, No. 2, pp. 181-190, (2004).
- [12]. Kong X., Gosselin C. M., *Type synthesis of 4-DoF SP-equivalent parallel manipulators: A virtual chain approach*, IFToMM J., Mechanism and Machine Theory, 41, pp. 1306-1329, (2006).
- [13]. Kong X., Gosselin C. M., *Generation of parallel manipulators with three translational degrees of freedom based on screw theory*, Proceedings of Symposium on Mechanisms, Machines and Mechatronics, Montreal, Canada (2001).
- [14]. Kong X., Gosselin C. M., *Type synthesis of parallel mechanisms*, Springer (2007).
- [15]. Freudenstein F., Alizade R.I., *On the degree of freedom of mechanisms with variable general constraint*, IV World IFToMM Congress, England, pp. 51-56, (1975).
- [16]. Alizade R.I., *On the degree of freedom of kinematic chain*, Az. Pol. Inst., Automation design of mechanisms, manipulator and robots, Baku, pp. 3-14, (1988).
- [17]. Alizade R.I. , Bayram C., *Structural synthesis of parallel manipulators*, IFToMM J. Mech. Mach. Theory 39, pp. 857-870, (2004).
- [18]. Alizade R.I., Can F.C., Gezgin E., *Structural synthesis of Euclidean platform robot manipulators with variable general constraints*, IFToMM J. Mech. Mach. Theory 43, pp. 1431-1449, (2008).

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